

# Nonlinear Circuits



## Circuits with nonlinear components

*Linear and Nonlinear Circuits, Chua, Desoer & Kuh 1987*  
*Chapter 2 section 1.1, 1.2, 1.4, 2.1, 2.2, and 2.3*

## 1.1 From Linear Resistor to Resistor

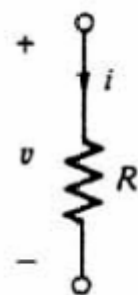


Figure 1.1 Symbol for a linear resistor with resistance  $R$ .

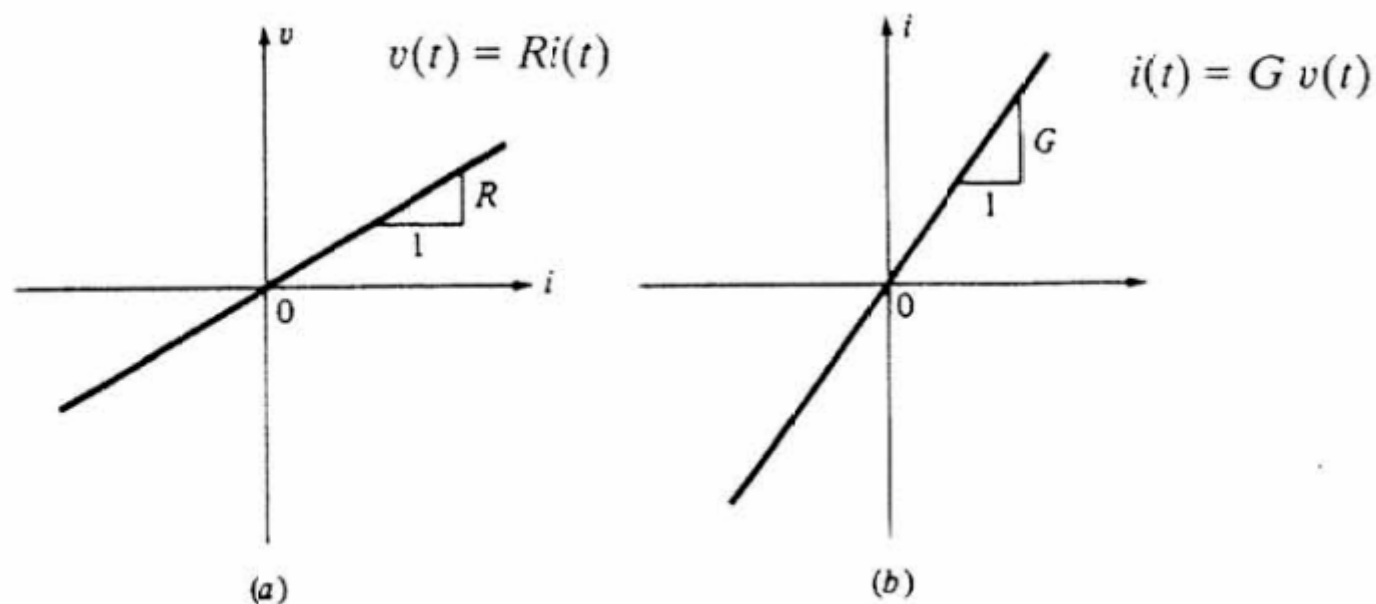
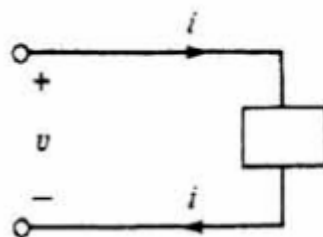


Figure 1.2 Linear resistor characteristic plotted (a) on the  $i$ - $v$  plane and (b) on the  $v$ - $i$  plane.



**Figure 1.3** A two-terminal element with  $v$  and  $i$  in the associated reference directions.

$$\mathcal{R}_R = \{(v, i): f(v, i) = 0\}$$

The linear resistor is a special case of a resistor in which

$$f(v, i) = v - Ri = 0 \quad \text{or} \quad f(v, i) = i - Gv = 0$$

A resistor which is not linear is called *nonlinear*.

## Open circuits and short circuits

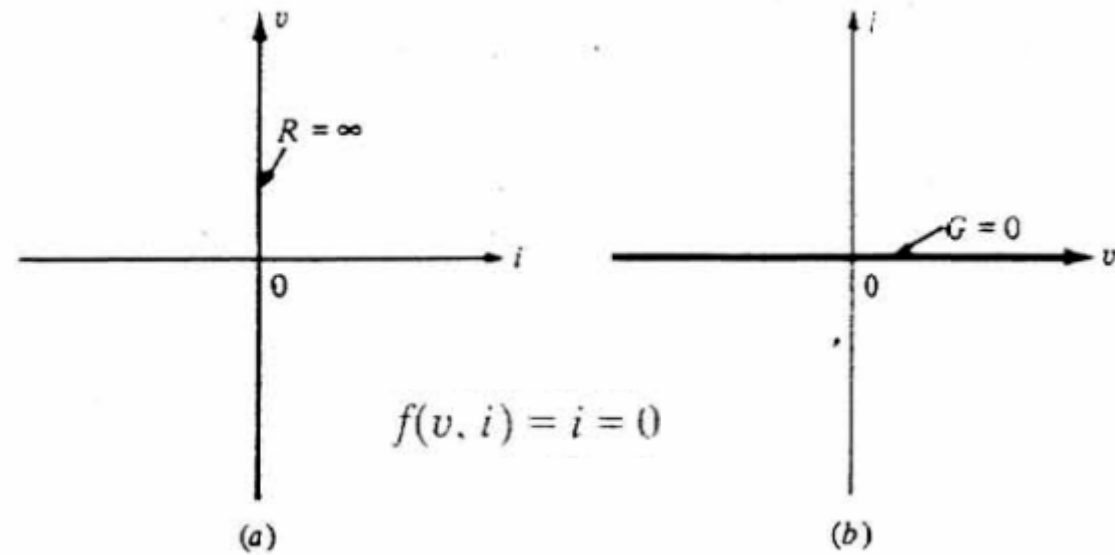


Figure 1.4 Characteristic of an open circuit.

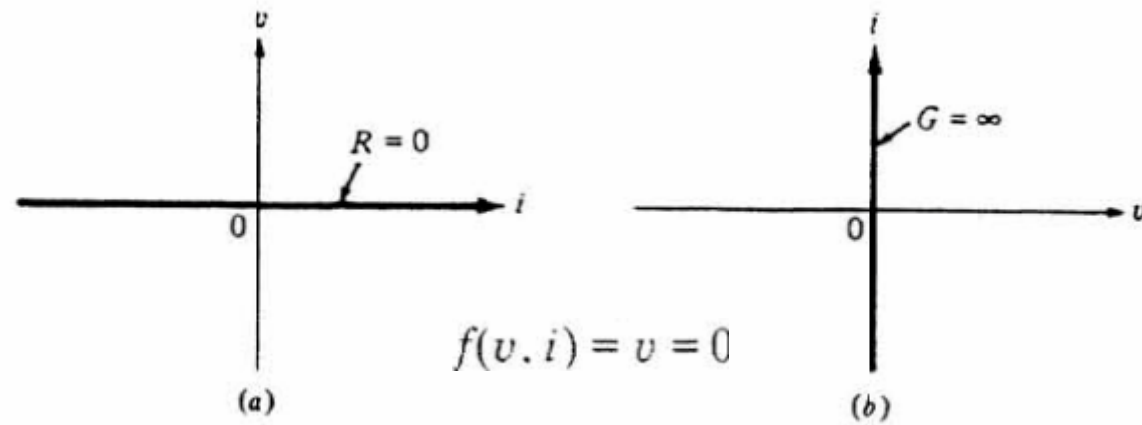


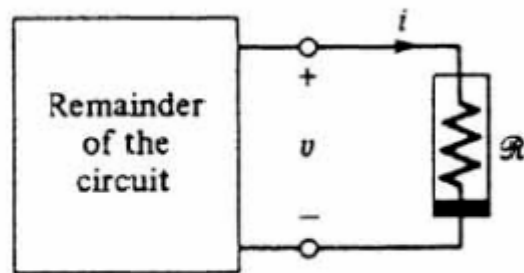
Figure 1.5 Characteristic of a short circuit.

## Power, passive resistors, active resistors, and modeling

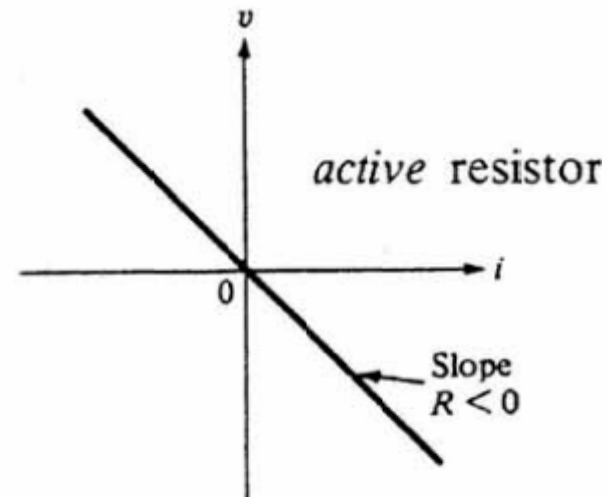
$$p(t) = v(t)i(t)$$

If the resistor is linear having resistance  $R$

$$p(t) = Ri^2(t) = Gv^2(t)$$

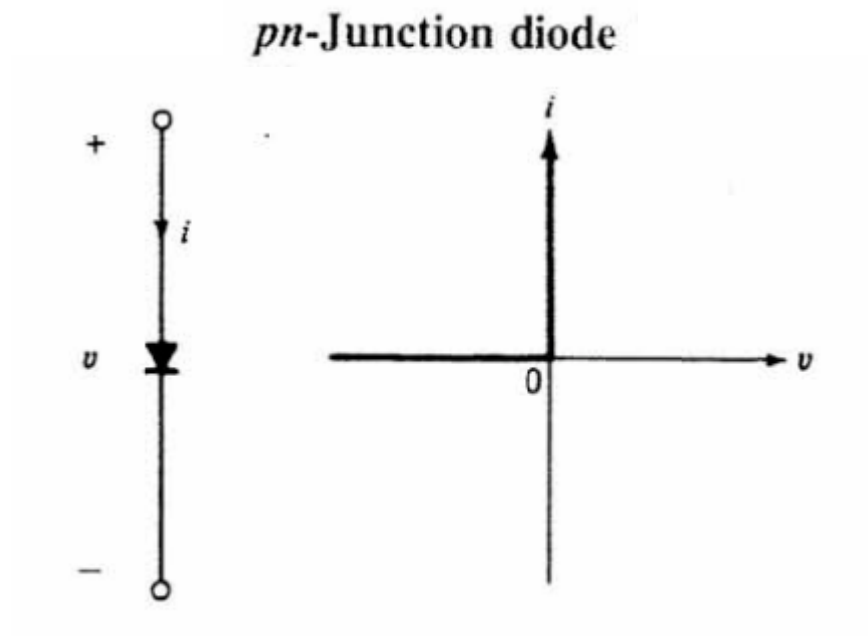


**Figure 1.6** Illustrating power delivered to a nonlinear resistor from the remainder of the circuit.



**Figure 1.7** Characteristic of a linear active resistor with resistance  $R < 0$ .

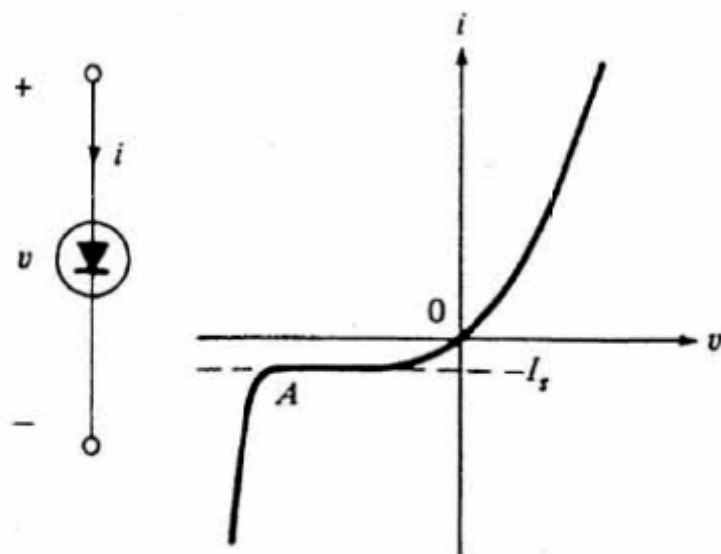
## 1.2 The Nonlinear Resistor



**Figure 1.8** Symbol for an ideal diode and its characteristic.

$$\mathcal{R}_{\text{ID}} = \{(v, i): vi = 0, i = 0 \text{ for } v < 0 \text{ and } v = 0 \text{ for } i > 0\}$$

$$i = I_s \left[ \exp\left(\frac{v}{V_T}\right) - 1 \right]$$



**Figure 1.9** Symbol for a *pn*-junction diode and its characteristic.



## Tunnel diode

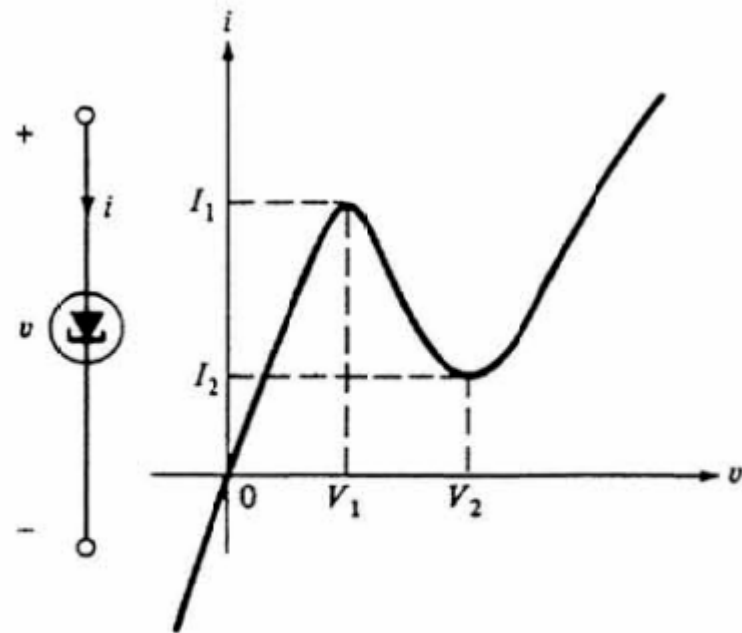


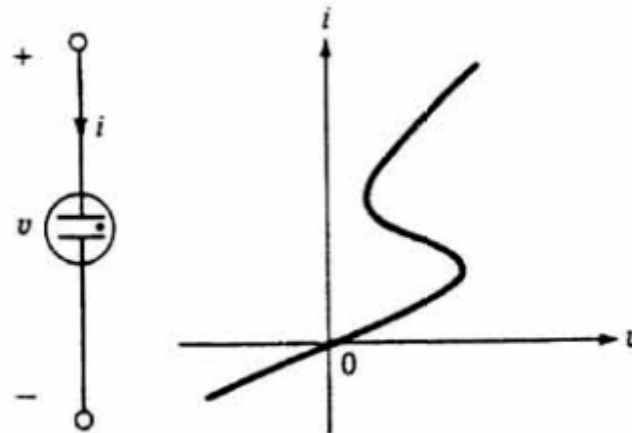
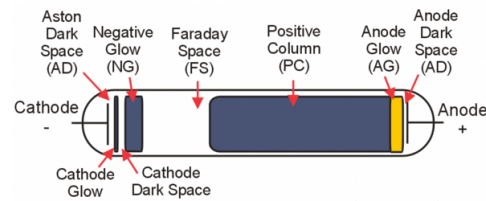
Figure 1.10 Symbol for a tunnel diode and its characteristic.

$$i = \hat{i}(v)$$

*voltage-controlled nonlinear resistor*



## Glow tube

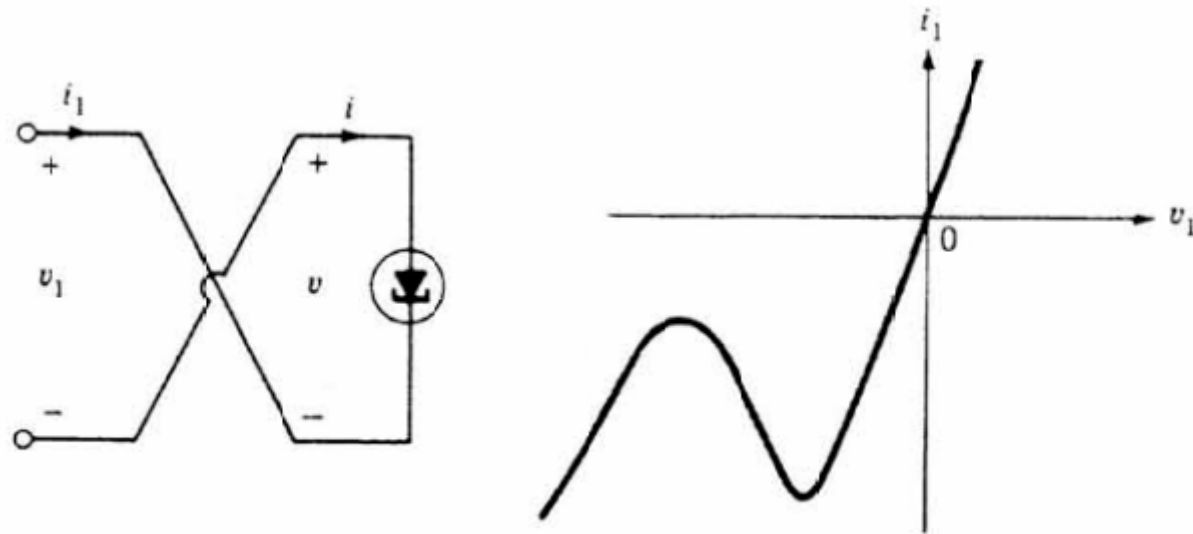


**Figure 1.11** Symbol for a glow tube and its characteristic.

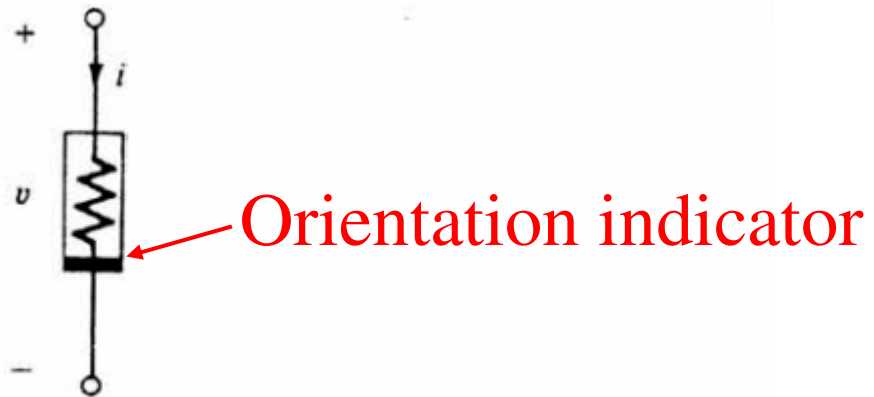
$$v = \hat{v}(i)$$

*current-controlled resistor*

### Bilateral property

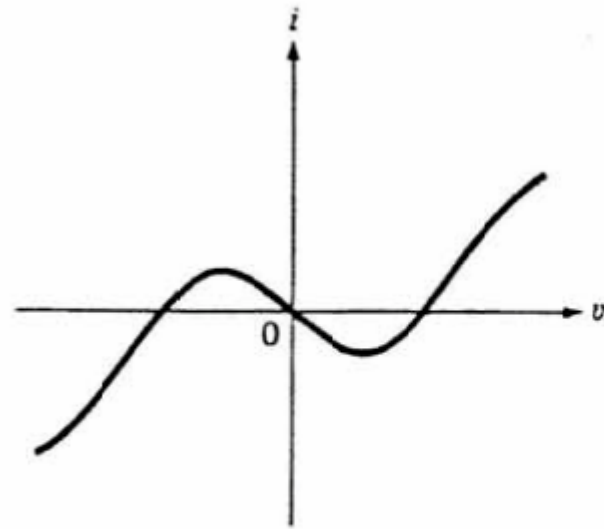


**Figure 1.12** Characteristic of a tunnel diode with its terminals turned around.



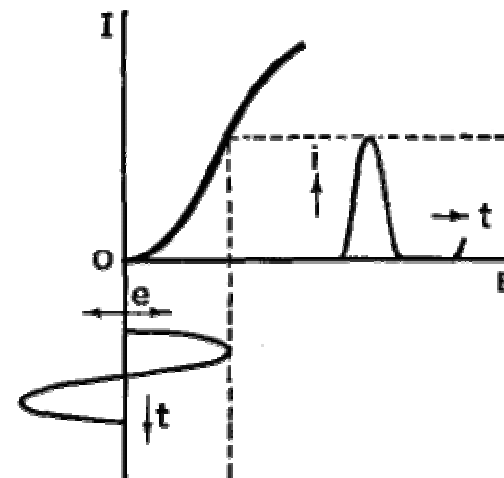
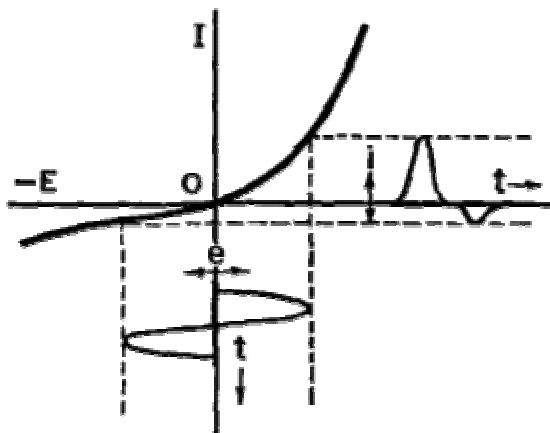
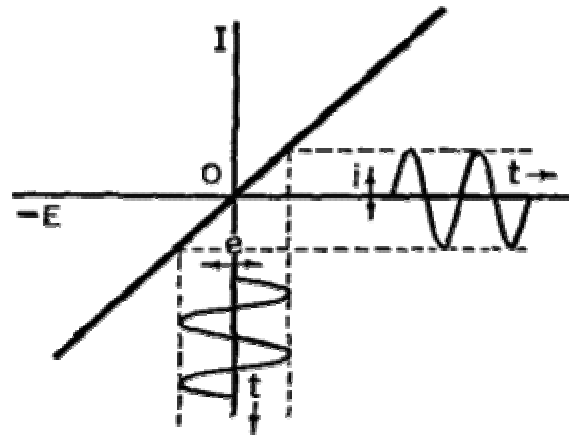
**Figure 1.13** Symbol for a nonlinear resistor.

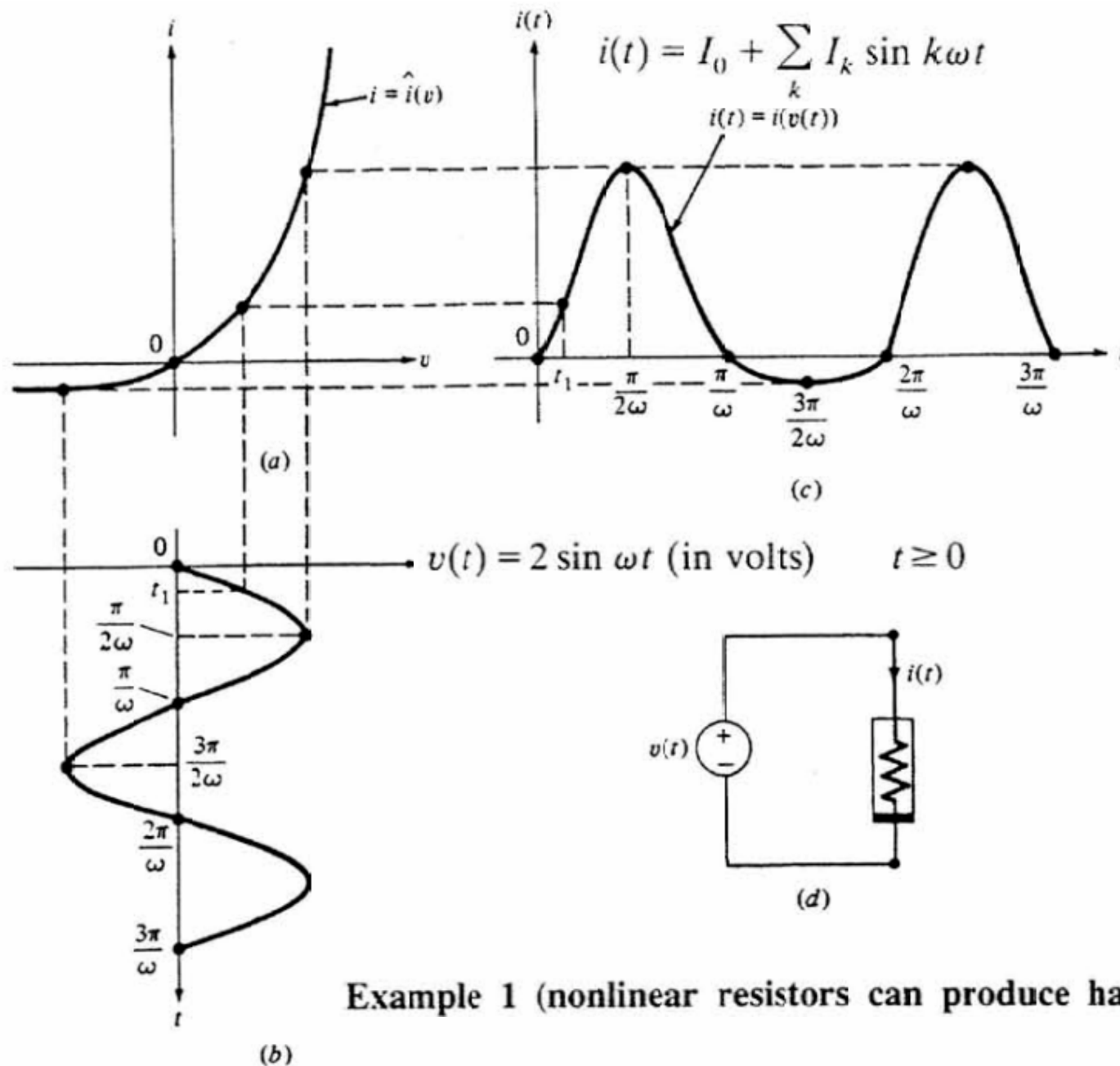
The characteristic of a *linear* resistor is always symmetric with respect to the origin. A circuit element with this kind of symmetry is called *bilateral*. A *bilateral resistor* satisfies the property  $f(v, i) = f(-v, -i)$  for all  $(v, i)$  on its characteristic. A nonlinear resistor may be bilateral, e.g., have the characteristic shown in Fig. 1.14.



**Figure 1.14**  $v$ - $i$  Characteristic of a bilateral nonlinear resistor.

**Simple circuits** Circuits containing nonlinear resistors have properties totally different from those which have only linear resistors. The following examples illustrate some of the differences.





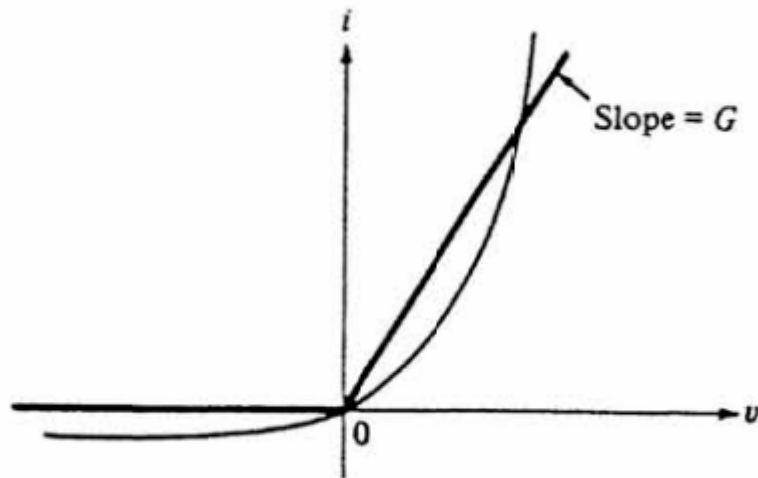
**Example 1 (nonlinear resistors can produce harmonics)**

**Figure 1.15** An example illustrating a special clipping property of nonlinear resistors; the negative half of the waveform has been clipped.

**Example 2 (piecewise-linear approximation)**

$$i(t) = \begin{cases} 2G \sin \omega t & \text{for } \frac{2n\pi}{\omega} \leq t \leq \frac{(2n+1)\pi}{\omega} \\ 0 & \text{for } \frac{(2n+1)\pi}{\omega} \leq t \leq \frac{(2n+2)\pi}{\omega} \end{cases}$$

where  $n$  runs through nonnegative integers.



**Figure 1.16** Piecewise-linear approximation of a nonlinear characteristic.

### Example 3 (homogeneity and additivity)

the currents in a linear resistor whose characteristic is

$$i_\ell = \hat{i}_\ell(v) = 0.1v$$

and in a nonlinear resistor whose characteristic is

$$i_n = \hat{i}_n(v) = 0.1v + 0.02v^3$$

$$v_1 = 1 \text{ V}, v_2 = k \text{ V, and } v_3 = v_1 + v_2 = 1 + k \text{ V.}$$

$$i_{\ell 2} = \hat{i}_\ell(kv_1) = k\hat{i}_\ell(v_1)$$

$$i_{\ell 3} = \hat{i}_\ell(v_1 + v_2) = \hat{i}_\ell(v_1) + \hat{i}_\ell(v_2)$$

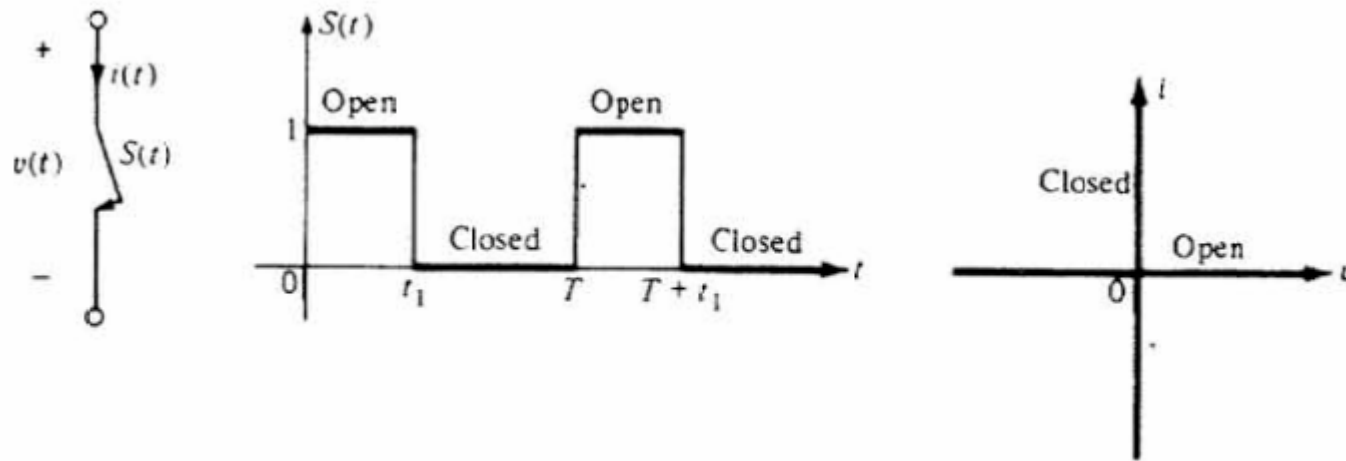
$$v_1 = 1 \text{ V}, v_2 = k \text{ V, and } v_3 = v_1 + v_2 \text{ V.}$$

$$i_{n2} = \hat{i}_n(kv_1) \neq k\hat{i}_n(v_1)$$

$$i_{n3} = \hat{i}_n(v_1 + v_2) \neq \hat{i}_n(v_1) + \hat{i}_n(v_2)$$

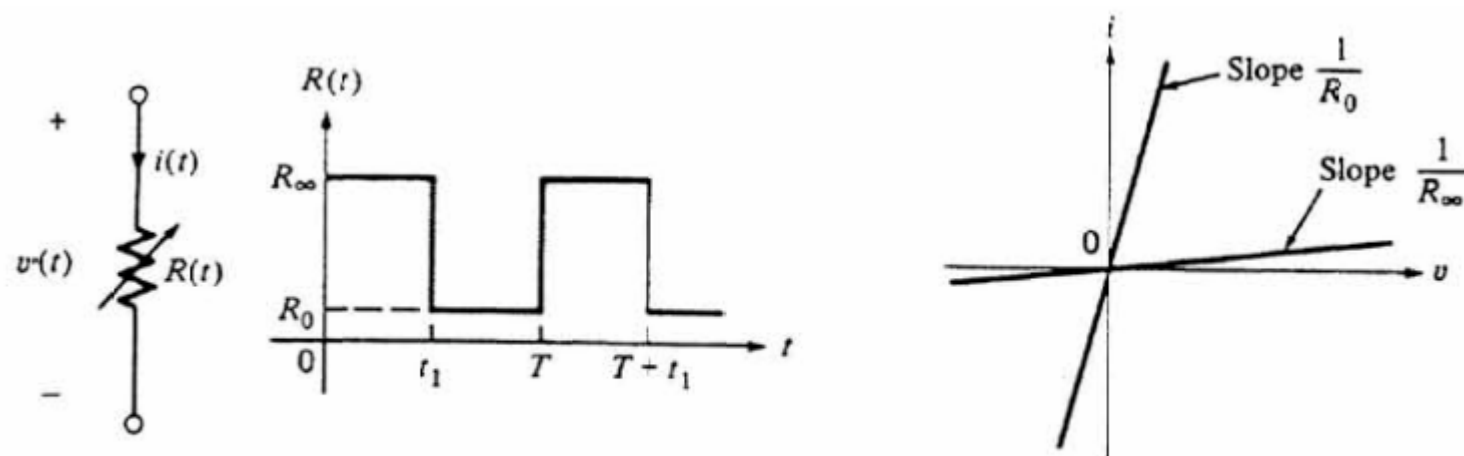
## 1.4 Time-Invariant and Time-Varying Resistors

$$v(t) = R(t)i(t) \quad \text{or} \quad i(t) = G(t)v(t)$$



**Figure 1.22** Symbol for a periodically operating switch and its characteristic. Here,  $S(t)$  denotes the "state" (i.e., position) of the switch.





**Figure 1.23** Symbol for a linear time-varying resistor and its characteristic.

**Example** Consider a linear time-varying resistor with  $v$ - $i$  characteristic

$$i(t) = G(t)v(t) \quad \text{and} \quad G(t) = G_a + G_b \cos \omega t$$

where the constants  $G_a$  and  $G_b$  satisfy the condition  $G_a > G_b$ ; consequently  $G(t) > 0$  for all  $t$ . The angular frequency  $\omega$  is also a constant. Let the voltage waveform be a sinusoid with angular frequency  $\omega_1$ . Then

$$v(t) = V_m \cos \omega_1 t$$

$$i(t) = G_a V_m \cos \omega_1 t + G_b V_m \cos \omega_1 t \cos \omega t$$

$$= G_a V_m \cos \omega_1 t + \frac{G_b V_m}{2} \cos(\omega + \omega_1)t + \frac{G_b V_m}{2} \cos(\omega - \omega_1)t$$



Generate 3 frequencies

## 2 SERIES AND PARALLEL CONNECTIONS

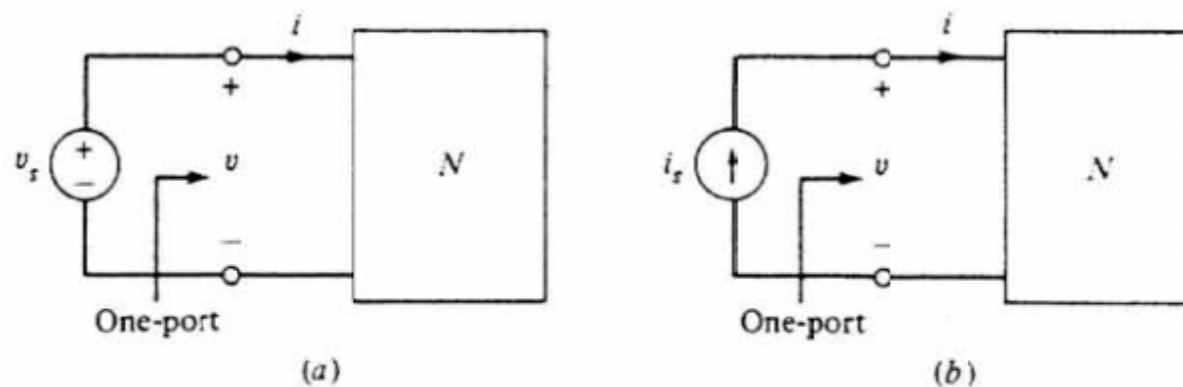
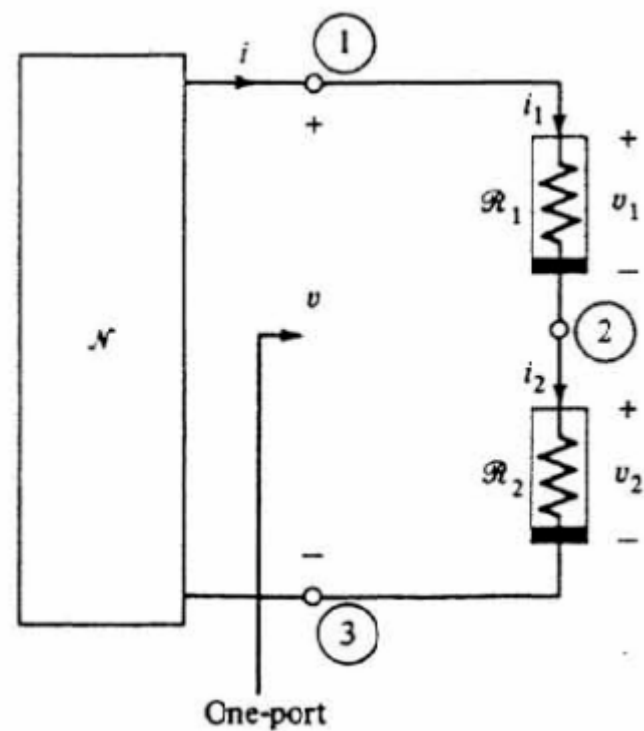


Figure 2.1 A one-port  $N$  driven (a) by an independent voltage source and (b) by an independent current source.

### 2.1 Series Connection of Resistors



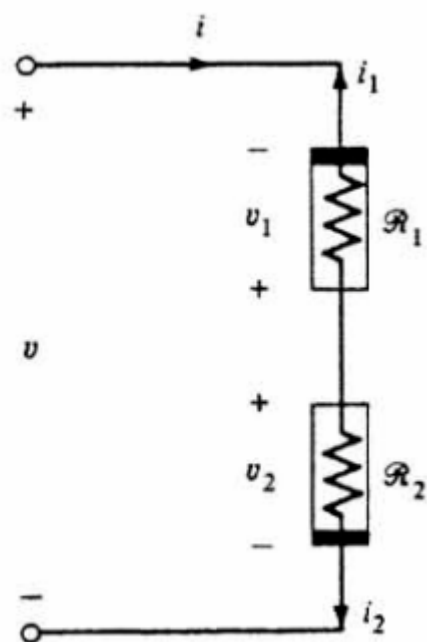
$$v_1 = \hat{v}_1(i_1) \quad \text{and} \quad v_2 = \hat{v}_2(i_2)$$

$$i = i_1 = i_2$$

$$v = v_1 + v_2$$

$$v = \hat{v}_1(i) + \hat{v}_2(i)$$

**Figure 2.2** Two nonlinear resistors connected in series together with the rest of the circuit  $\mathcal{N}$ .



$$\hat{v}(i) = -\hat{v}_1(-i) + \hat{v}_2(i)$$

**Figure 2.3** Series connection of  $\mathcal{R}_1$  and  $\mathcal{R}_2$  with the terminals of  $\mathcal{R}_1$  turned around.

### Example 1 (a battery model)

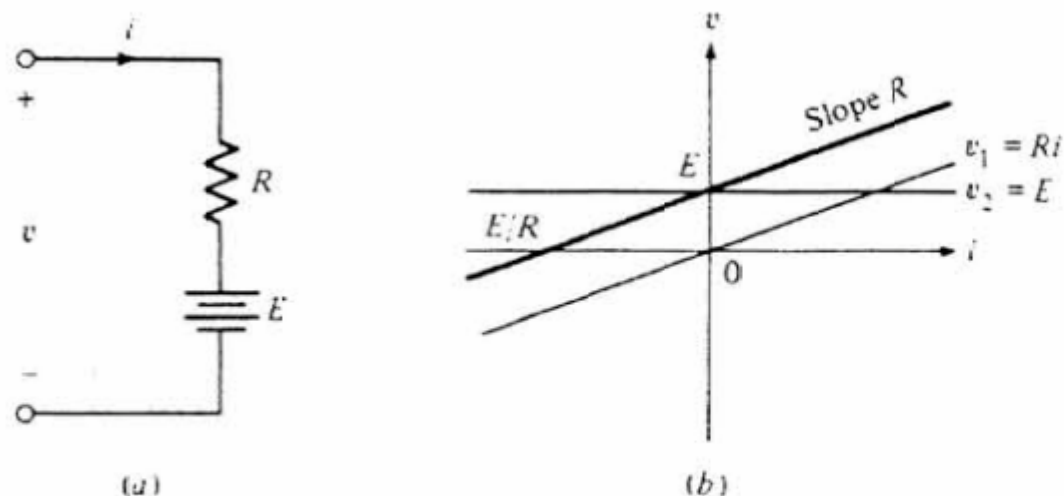


Figure 2.4 (a) Series connection of a linear resistor and a dc voltage source, and (b) its driving-point characteristic.

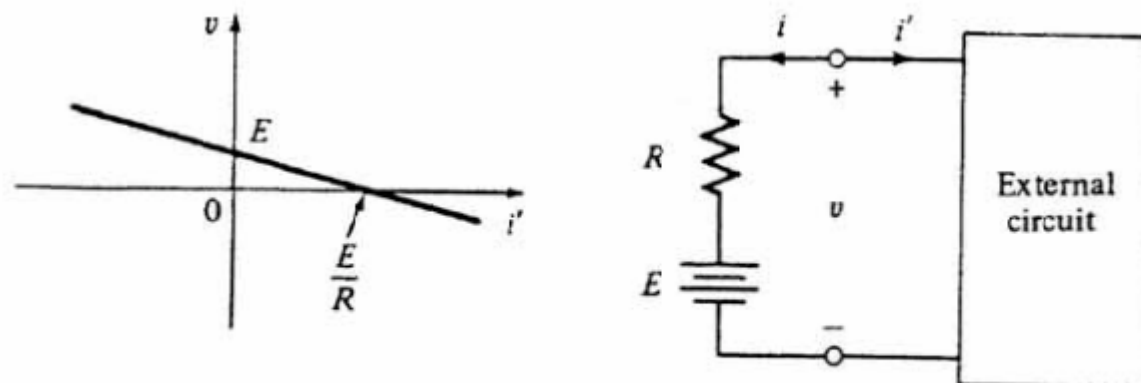
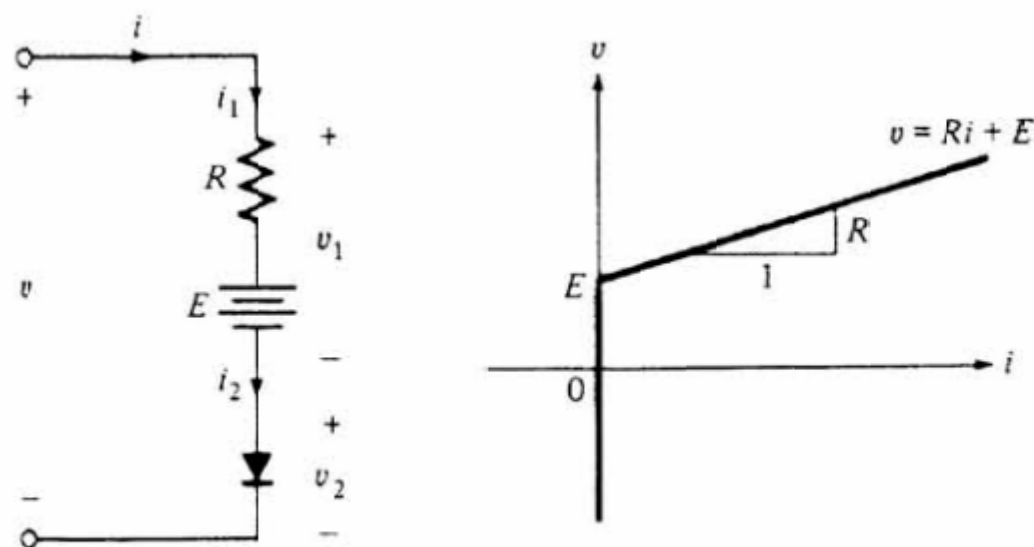


Figure 2.5 Characteristic of a real battery plotted on the  $i'$ - $v$  plane and the external circuit connection.

### Example 2 (ideal diode circuit)



**Figure 2.6** Series connection of a battery with an ideal diode and the driving-point characteristic of the resulting one-port.

$$v = v_1 = Ri + E \quad \text{for } i > 0$$

$$v = E + v_2 \quad \text{and} \quad i = 0 \quad \text{for } v_2 \leq 0$$

### Example 5 (graphic method)

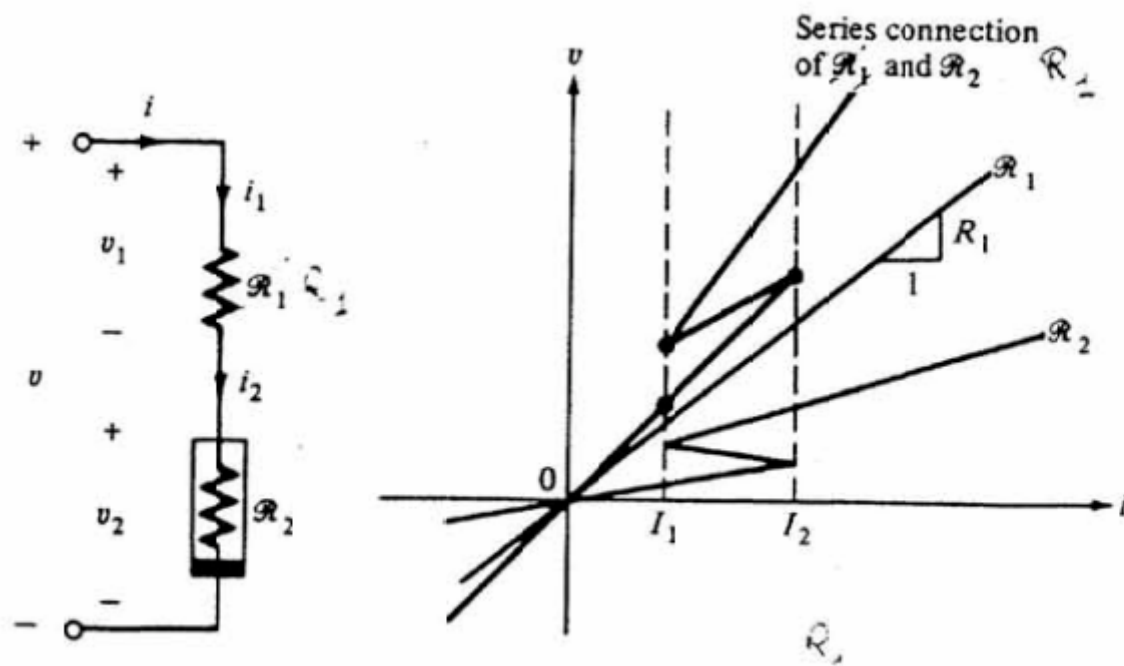


Figure 2.9 Series connection of a linear resistor  $\mathcal{R}_1$  and a voltage-controlled resistor  $\mathcal{R}_2$ .

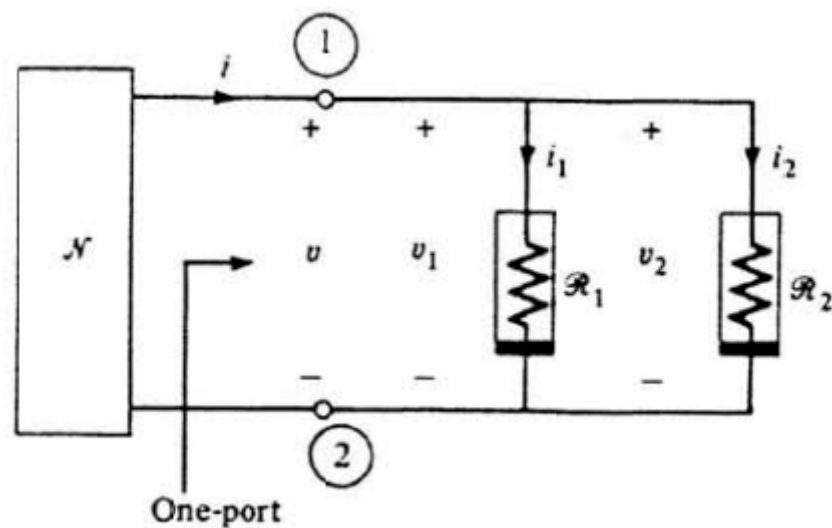
$$v_1 = R_1 i_1 \quad \text{and} \quad i_2 = \hat{i}_2(v_2)$$



**Summary of series connection** The key concepts used in obtaining the driving-point characteristic of a one-port formed by the series connection of two-terminal resistors are

1. KCL forces all branch currents to be equal to the port current.
2. KVL requires the port voltage  $v$  to be equal to the sum of the branch voltages of the resistors.
3. If each resistor is current-controlled, the resulting driving-point characteristic of the one-port is also a current-controlled resistor.

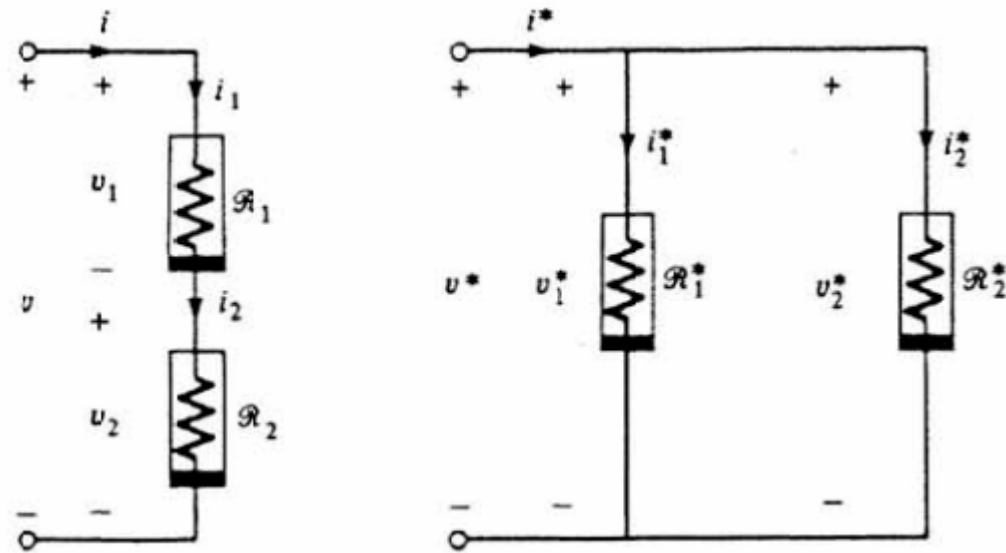
## 2.2 Parallel Connection of Resistors



**Figure 2.10** Two nonlinear resistors in parallel together with the rest of the circuit  $\mathcal{N}$ .

$$i_1 = \hat{i}_1(v_1) \quad \text{and} \quad i_2 = \hat{i}_2(v_2)$$

$$i = \hat{i}_1(v) + \hat{i}_2(v)$$

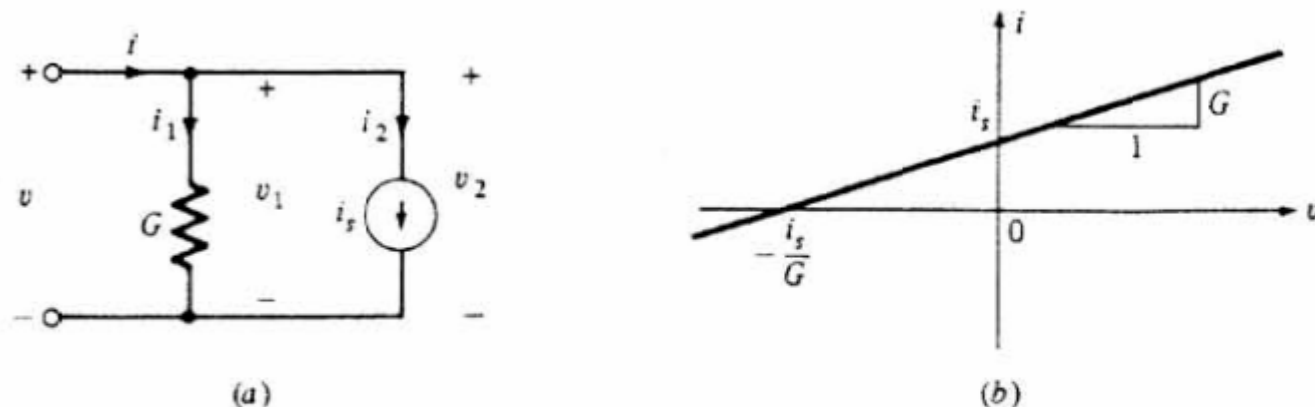


**Figure 2.11** A circuit  $\mathcal{N}$  and its dual  $\mathcal{N}^*$ .

**Table 2.1 Dual terms**

$S$	$S^*$
Branch voltage	Branch current
Current-controlled resistor	Voltage-controlled resistor
Resistance	Conductance
Open circuit	Short circuit
Independent voltage source	Independent current source
Series connection	Parallel connection
KVL	KCL
Port voltage	Port current

### Example 1 (dual one-port and equivalent one-port)



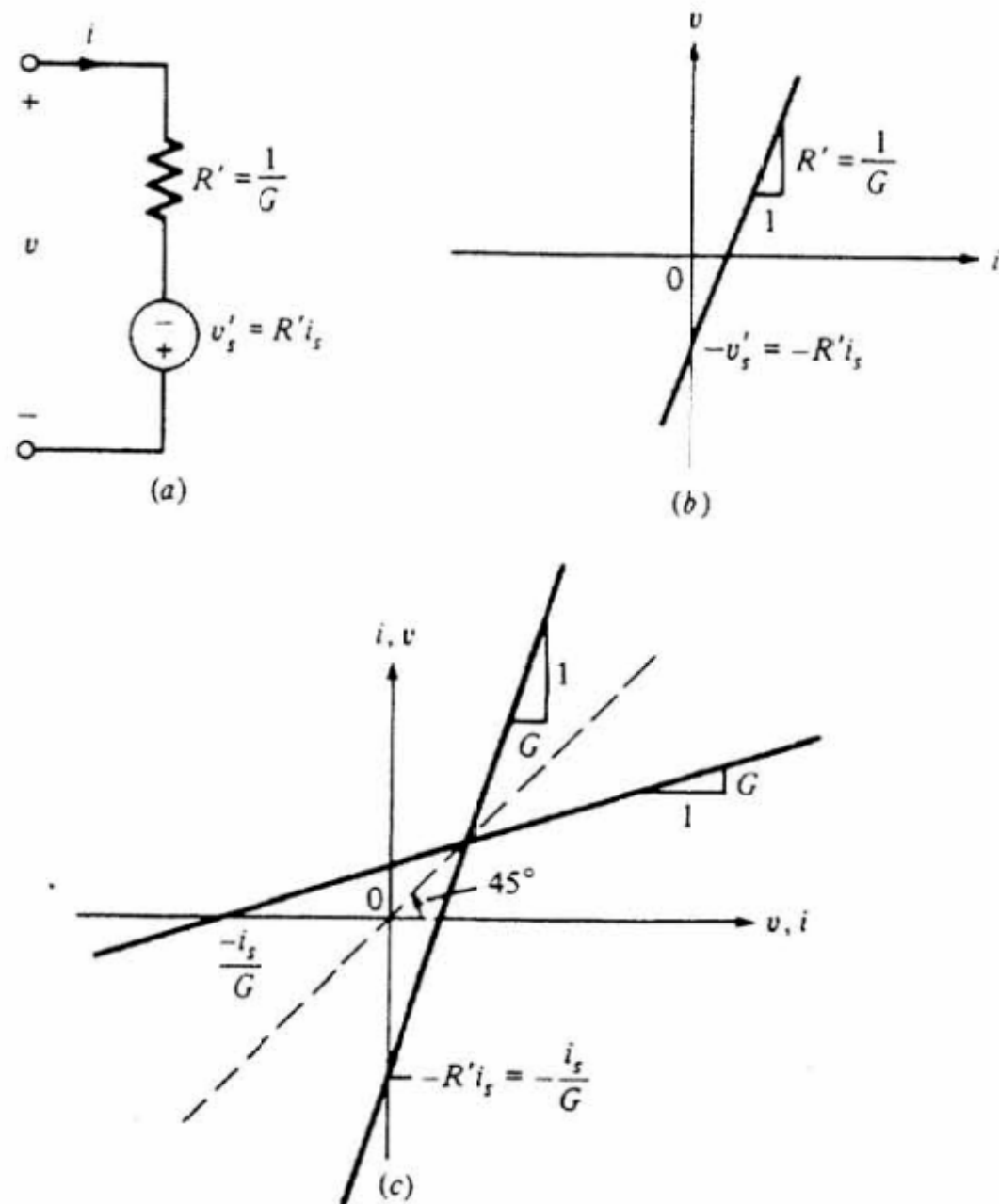
**Figure 2.12** (a) Parallel connection of a linear resistor and an independent current source. (b) The driving-point characteristic of the resulting one-port.

$$i_1 = Gv_1 \quad \text{and} \quad i_2 = i_s$$

$$i = Gv + i_s$$

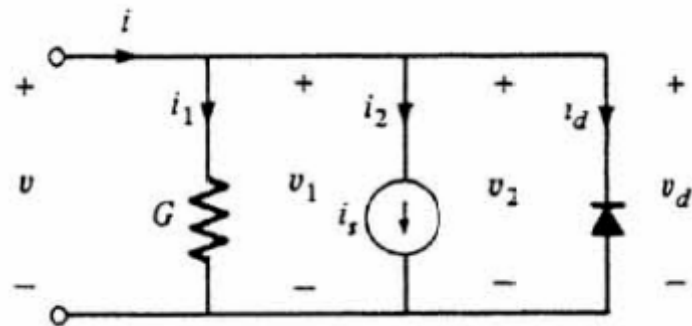
$$R'i = v + R'i_s$$

$$v = R'i - v'_s$$

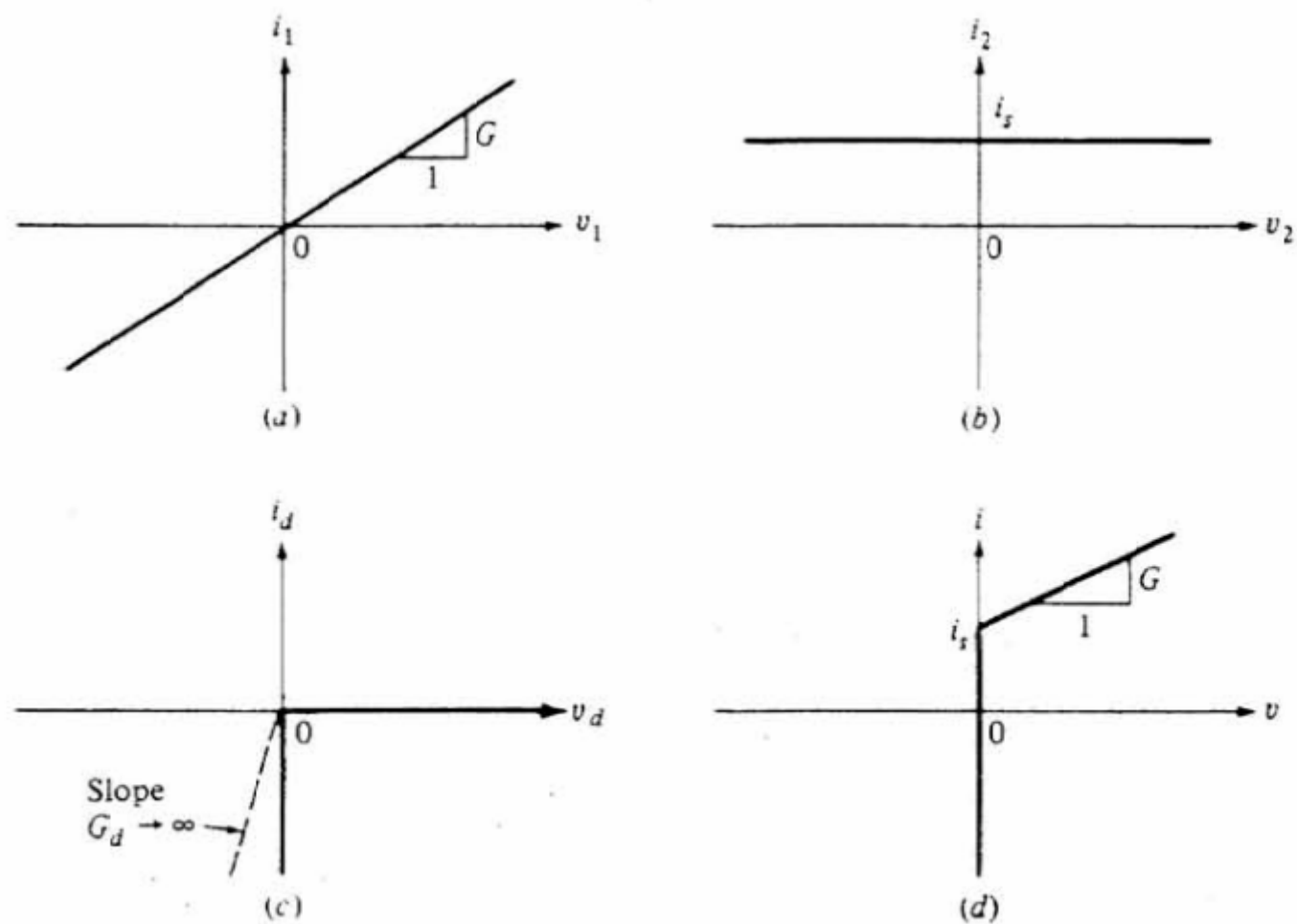


**Figure 2.13** The one-port in (a) is equivalent to that of Fig. 2.12a since they have the same driving-point characteristics.

**Example 2 (more on the ideal diode)**



**Figure 2.14** Parallel connection of a linear resistor, a current source, and an ideal diode.



**Figure 2.15** Branch  $v$ - $i$  characteristics of (a) a linear resistor, (b) a current source, and (c) an ideal diode. (d) The resulting one-port characteristic.

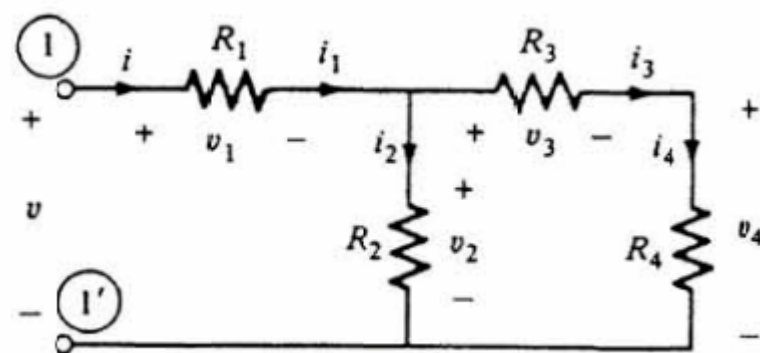


**Summary of parallel connection** The key concepts used in obtaining the driving-point characteristic of a one-port formed by the parallel connection of two-terminal resistors are

1. KVL forces all branch voltages to be equal.
2. KCL requires the port current  $i$  to be equal to the sum of the branch currents of the resistors.
3. If each resistor is voltage-controlled, the resulting driving-point characteristic of the one-port is also a voltage-controlled resistor.

## 2.3 Series-Parallel Connection of Resistors

**Example 1** (series-parallel connection of linear resistors)



**Figure 2.17** A ladder circuit with linear resistors.

$$v_2 = v_3 + v_4 = (R_3 + R_4)i_3$$

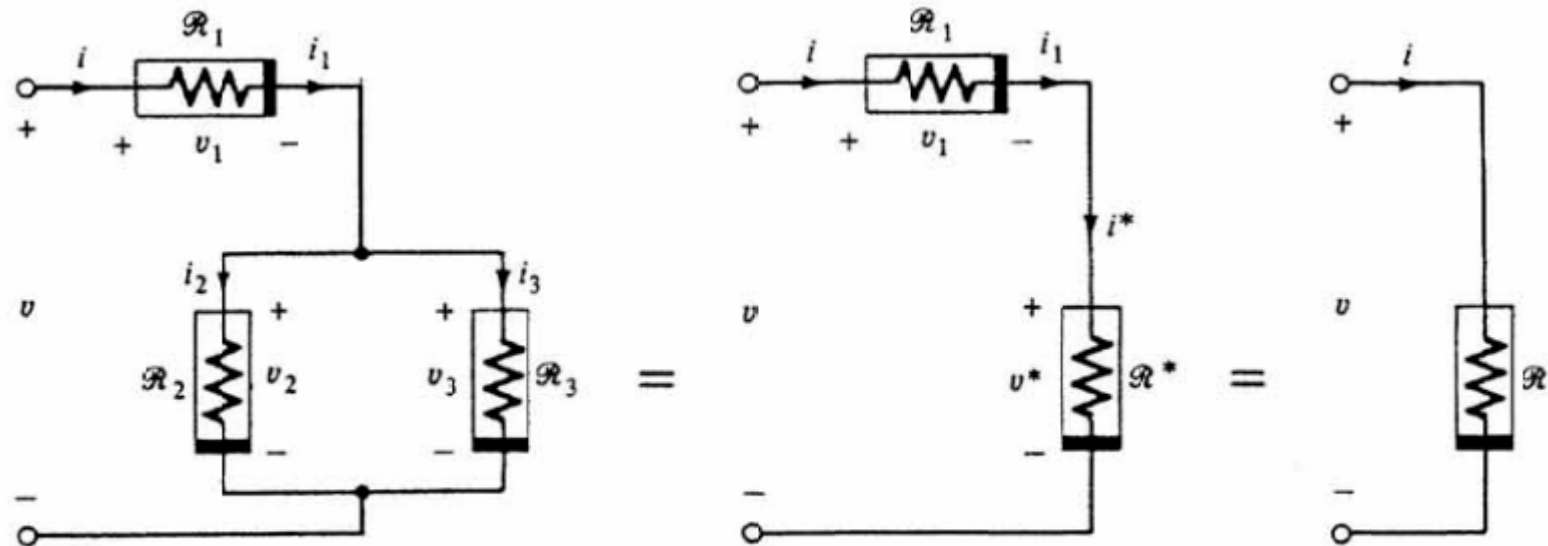
$$i_1 = i_2 + i_3 = G_2 v_2 + \frac{1}{R_3 + R_4} v_2 = \left( G_2 + \frac{1}{R_3 + R_4} \right) v_2$$

$$v = v_1 + v_2 = R_1 i_1 + \frac{1}{G_2 + 1/(R_3 + R_4)} i_1$$

where

$$R \triangleq R_1 + \frac{1}{G_2 + 1/(R_3 + R_4)}$$

**Example 2 (series-parallel connection of nonlinear resistors)**



**Figure 2.19** Reduction of a ladder circuit with nonlinear resistors.

$\mathcal{R}_2$  and  $\mathcal{R}_3$  are voltage-controlled

$$i_2 = \hat{i}_2(v_2) \quad \text{and} \quad i_3 = \hat{i}_3(v_3)$$

$$i^* = g(v^*)$$

$$g(v^*) = \hat{i}_2(v^*) + \hat{i}_3(v^*) \quad \text{for all } v^*$$

$\mathcal{R}_1$  is current-controlled

$$v_1 = \hat{v}_1(i_1)$$

$$v^* = g^{-1}(i^*) \quad \text{for all } i^*$$

$$i = i_1 = i^* \text{ and } v = v_1 + v^*$$

$$v = \hat{v}(i)$$

where

$$\hat{v}(i) = \hat{v}_1(i) + g^{-1}(i) \quad \text{for all } i$$

In this problem, one key step is the determination of the inverse function  $g^{-1}(\cdot)$ . The question is therefore whether the inverse exists. If it does not, the characteristic of  $\mathcal{R}$  cannot be written as in Eq. (2.24) because it is not current-controlled. One simple criterion which guarantees the existence of the inverse is that the  $v$ - $i$  characteristic is *strictly monotonically increasing*, i.e., the slope,  $g'(v^*)$  is positive for all  $v^*$

REMARK The characteristic of the one-port shown in Fig. 2.19 can always be represented parametrically. Indeed, we have

$$i = i_1 = i^* \quad \text{and} \quad v = v_1 + v^*$$

Hence, using  $v^*$  as a parameter, we obtain

$$i = g(v^*)$$

$$v = \hat{v}_1[g(v^*)] + v^*$$

# 1 TWO-TERMINAL CAPACITORS AND INDUCTORS

## 1.1 $q$ - $v$ and $\phi$ - $i$ characteristics

$$f_C(q, v) = 0$$

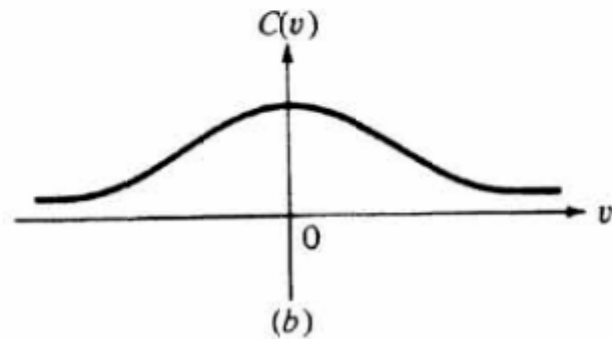
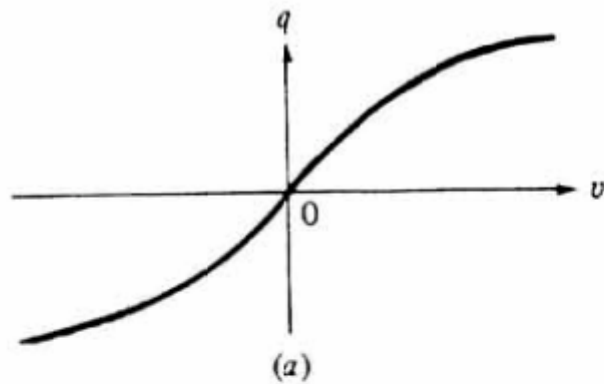


Figure 1.3 Nonlinear  $q$ - $v$  characteristic.

$$f_L(\phi, i) = 0$$

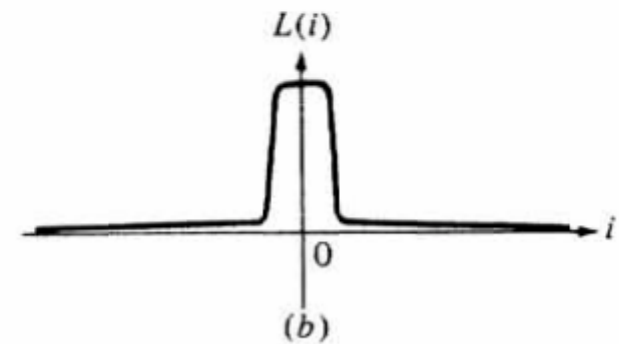
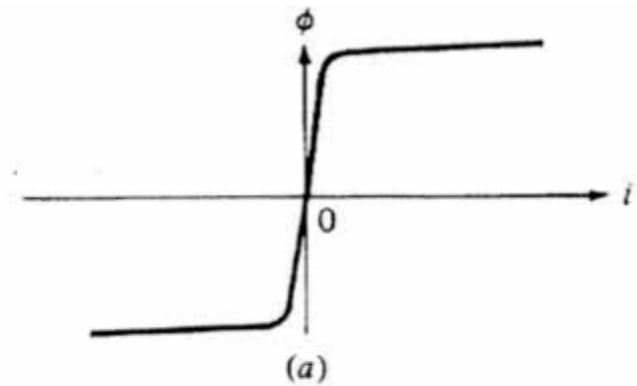
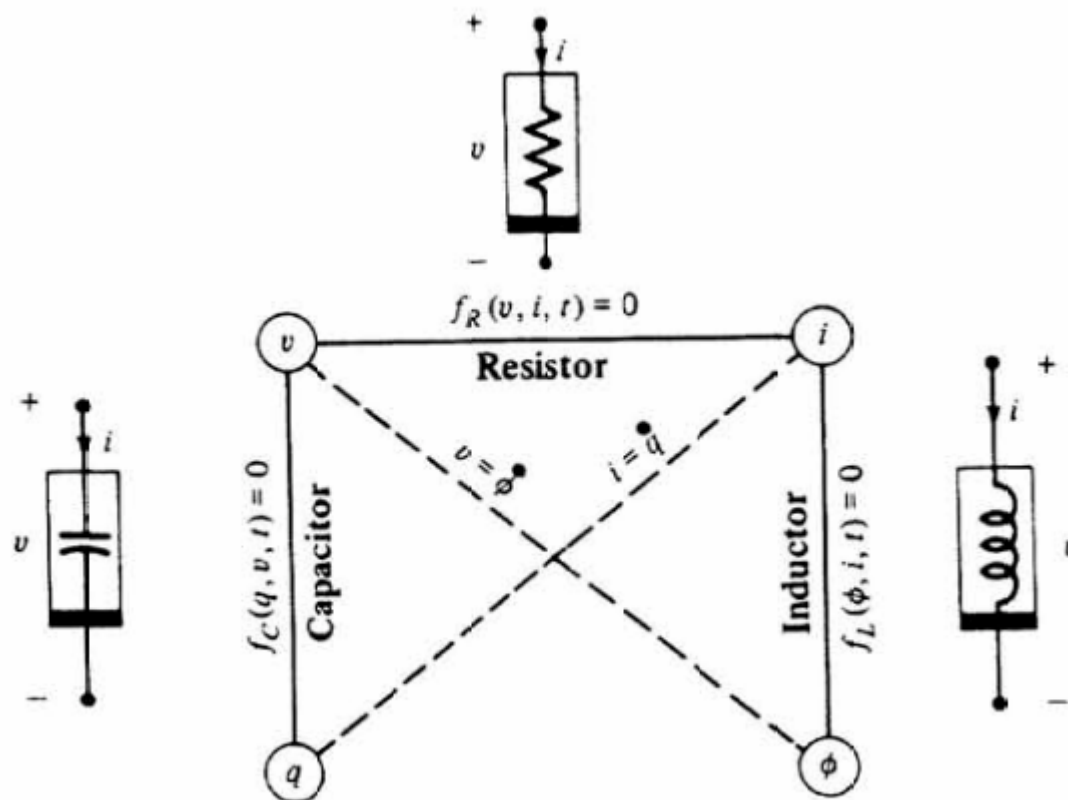


Figure 1.4 Nonlinear  $\phi$ - $i$  characteristic.



**Figure 1.9** Basic circuit element diagram.

<sup>11</sup> A fourth nonlinear two-terminal element called the *memristor* is defined by the remaining relationship between  $q$  and  $\phi$ . This circuit element is described in L. O. Chua, "Memristor—The Missing Circuit Element," *IEEE Trans. on Circuit Theory*, vol. 18, pp. 507–519, September 1971.